



# Optimized WESP and/or RTO System Design

## Refurbish Instead of Replace

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# Refurbish and / or upgrade of existing WESP and/or RTOs

Correct problem areas only and reuse existing:

- foundations
- power wiring
- Burners and/or piping
- Other items that are acceptable

Optimize and up grade with new features:

- Replace and/or repair needed components identified from inspection.
- Replace hydraulic butterfly with pneumatic poppet valves
- Replace media cold face support susceptible to failure
- Add flow **distribution nozzles** with uniform air distribution
- Add on line bake out system, **no production down time**
- Add thermal Energy alignment for Energy savings

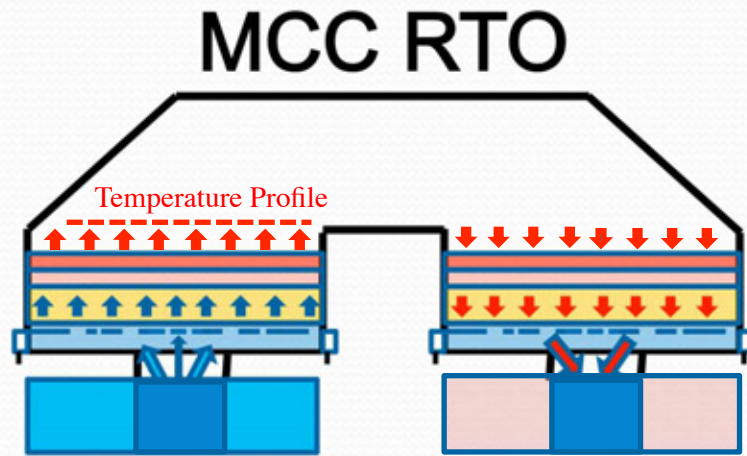


# Common issues with existing older WESP & Regenerative Thermal Oxidizers (RTOs) which can be corrected:

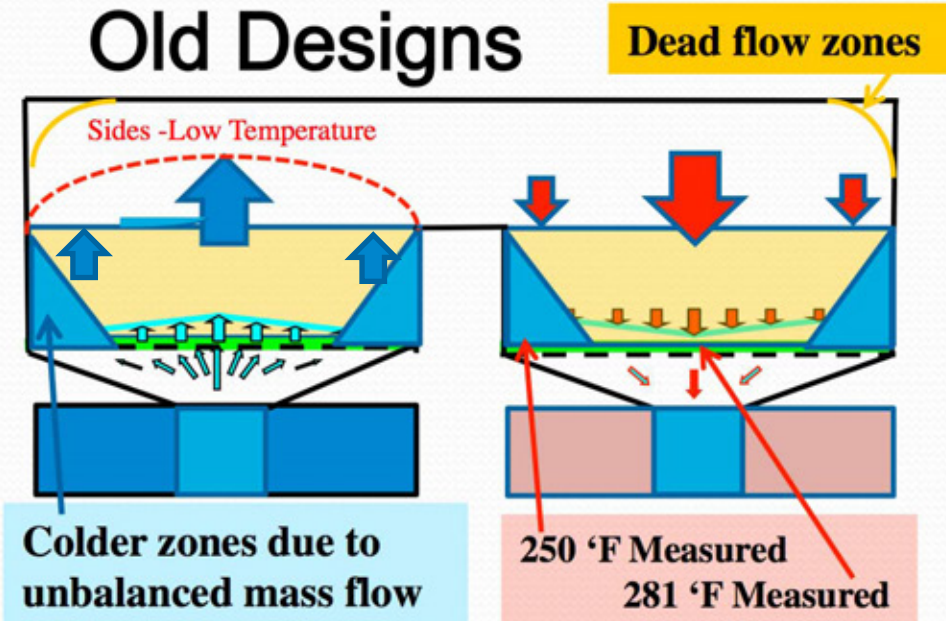
1. Poor Uniform Air Flow Distribution and Temperature Profile
2. Poor water management
3. Heat Exchange Media Failure
4. Chloride-induced stress corrosion cracking Failure
  - a. Insulation anchor Failure
  - b. Media support
5. Media Support Failure
6. Flow Control Valve Failure



# 1. Uniform air flow with Uniform temperature... Minimize un-combusted VOC



- § uniform flow
- § Cold Face distribution nozzle (proprietary)
- § uniform temperature control
  - § Multiple burners
  - § Auto-thermal alignment control (proprietary)

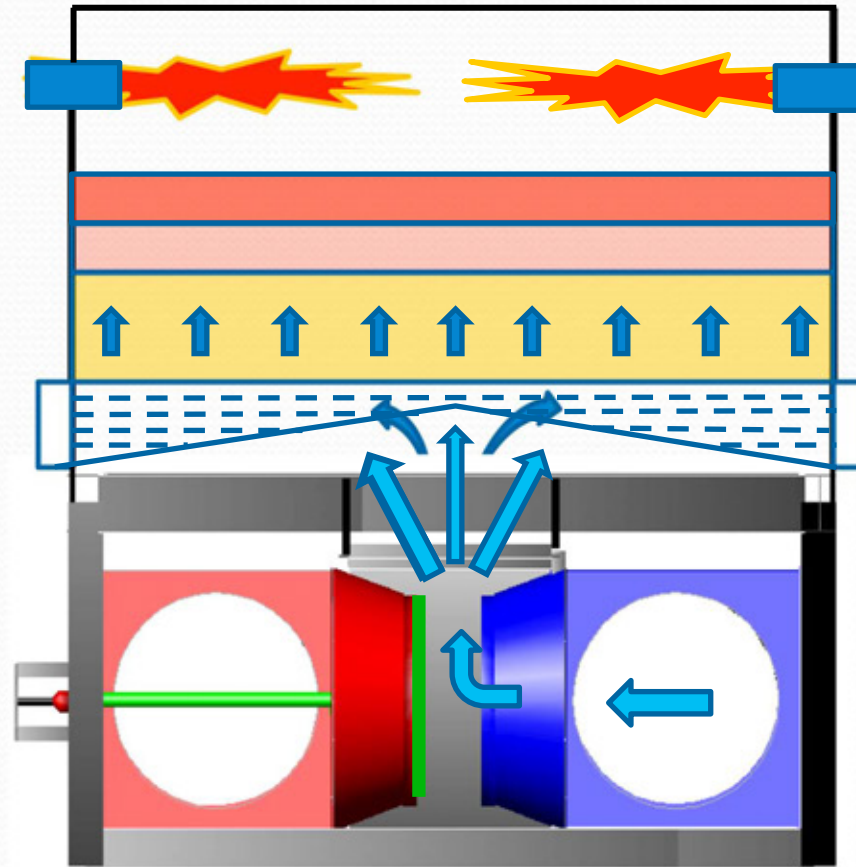


- Increase CO due to non uniform temperature
  - Increased fuel consumption (reduced TER)
- Reduced DRE due to both non uniform flow & temperature
- 2 to 2.5 times larger un-combusted cold face chamber dirty volume exhausted



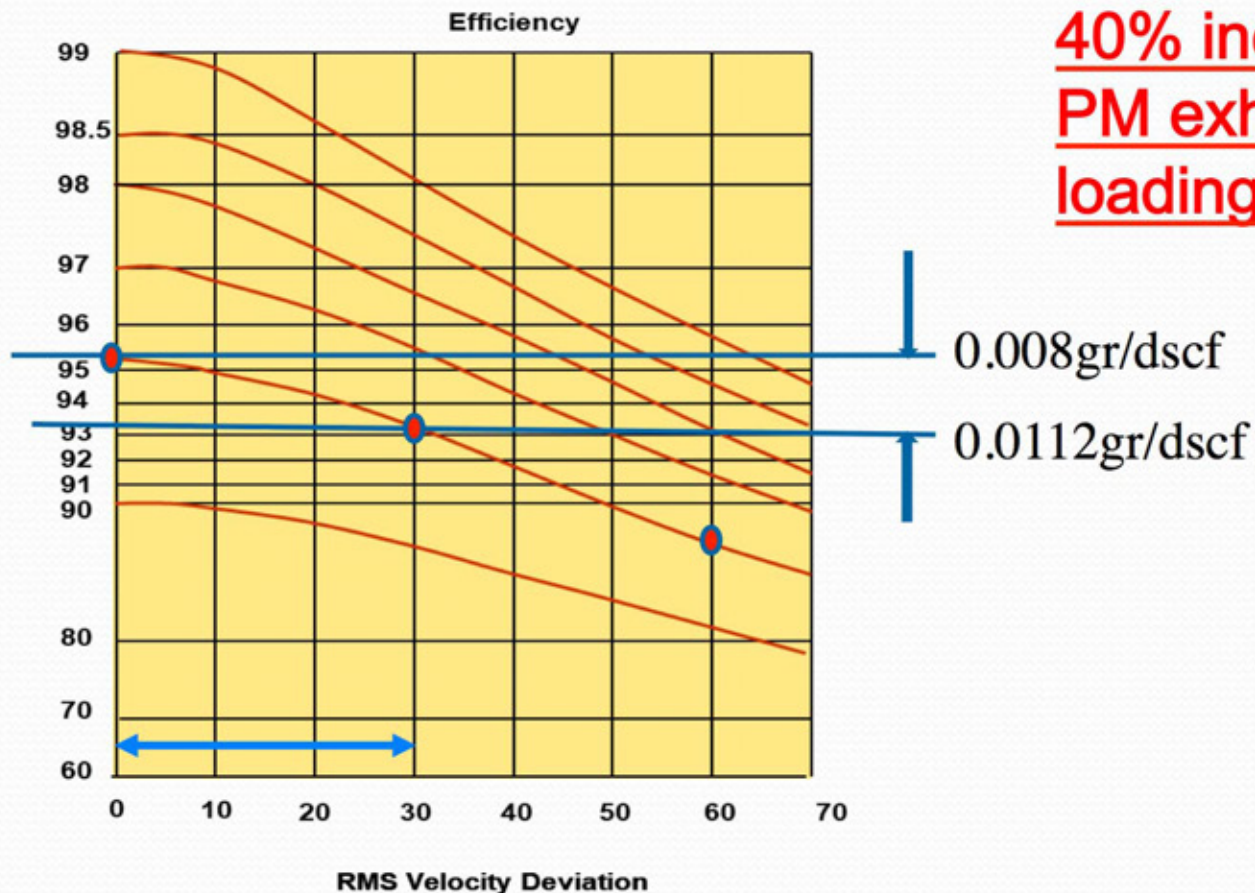
## Uniform Air Flow & Temperature Distribution Key to Large Wood RTO UNIT Performance

- Ø Media entry nozzle distributor (can be installed in existing RTOs)
- Ø Symmetrical Center media bed entry & exit
- Ø Contour valve entry
- Ø Over sized valves
- Ø Multi-layered media
- Ø Multi-Burner control





# WESP Uniform Air Flow, both up & down Flow, Key for Maximum Performance



40% increase in  
PM exhaust  
loading to RTO

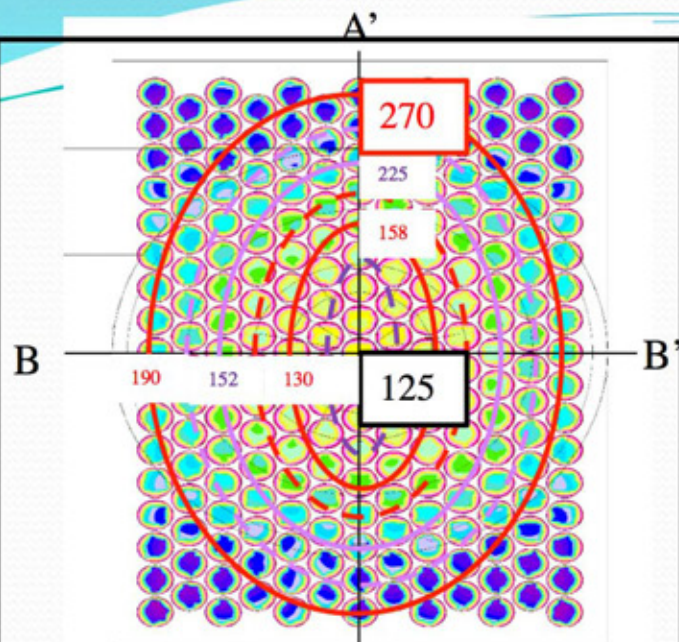


Down Flow

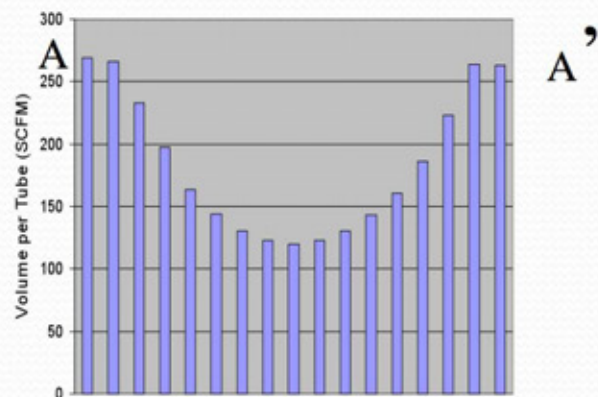


Up Flow



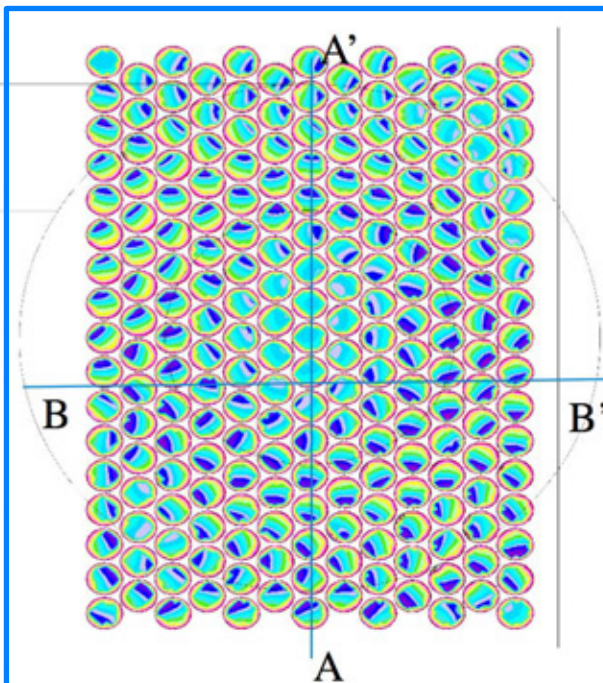


**Before Correction**

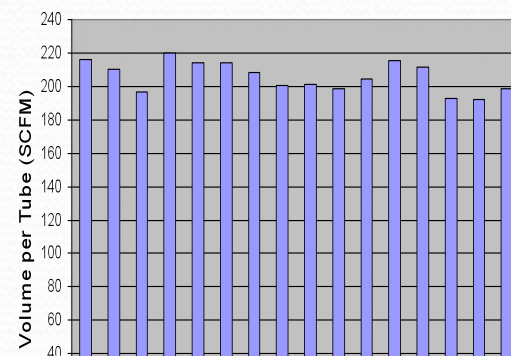


Tube volume variation:  $\pm \sim 70\%$

April 13, 2018



**After Correction**



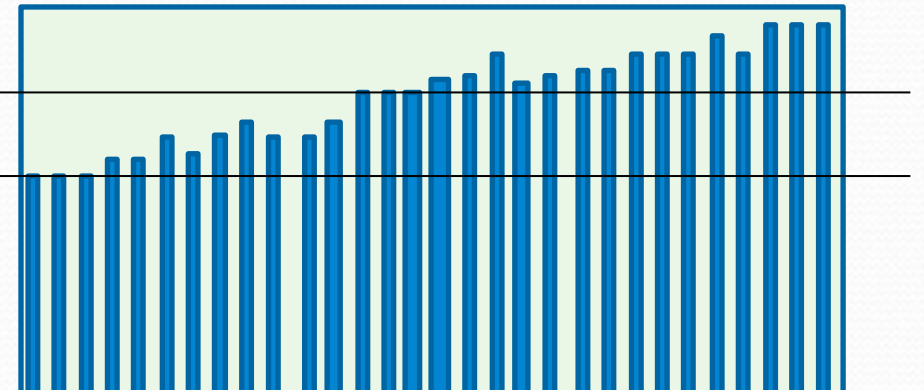
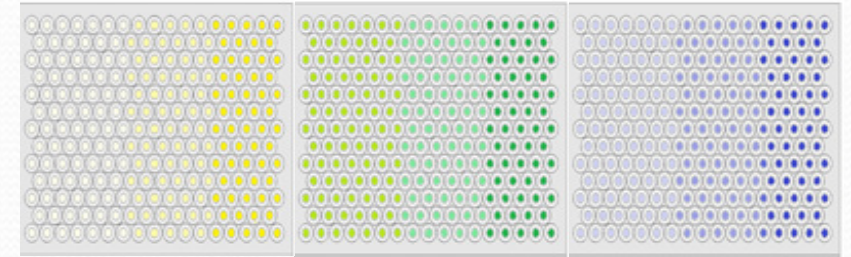
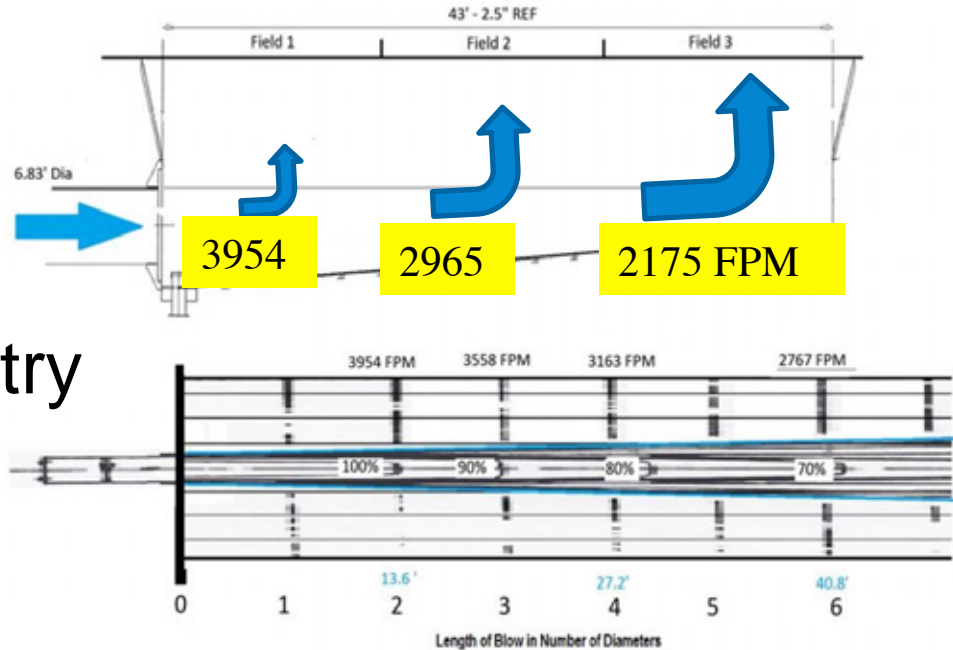
Tube volume variation:  $\pm 10\%$

7

**Plan view  
of WESP  
tube flow  
distribution**



# Elevation view of WESP tube flow distribution



+/- 22% in tube flow =  
Reduced efficiency

High Entry  
Flow  
Velocity

WESP inlet plenum Velocity					
145,000	ACFM flow	WESP inlet duct dia 82"	distance from inlet duct (ft)	Air Velocity	
	Plenum inlet Velocity	6.83		3,954	FPM
	5 dia into plenum		34	2,965	FPM
	10 dia into plenum		68	2,175	FPM



# Poor WESP performance results in condensable/PM build up



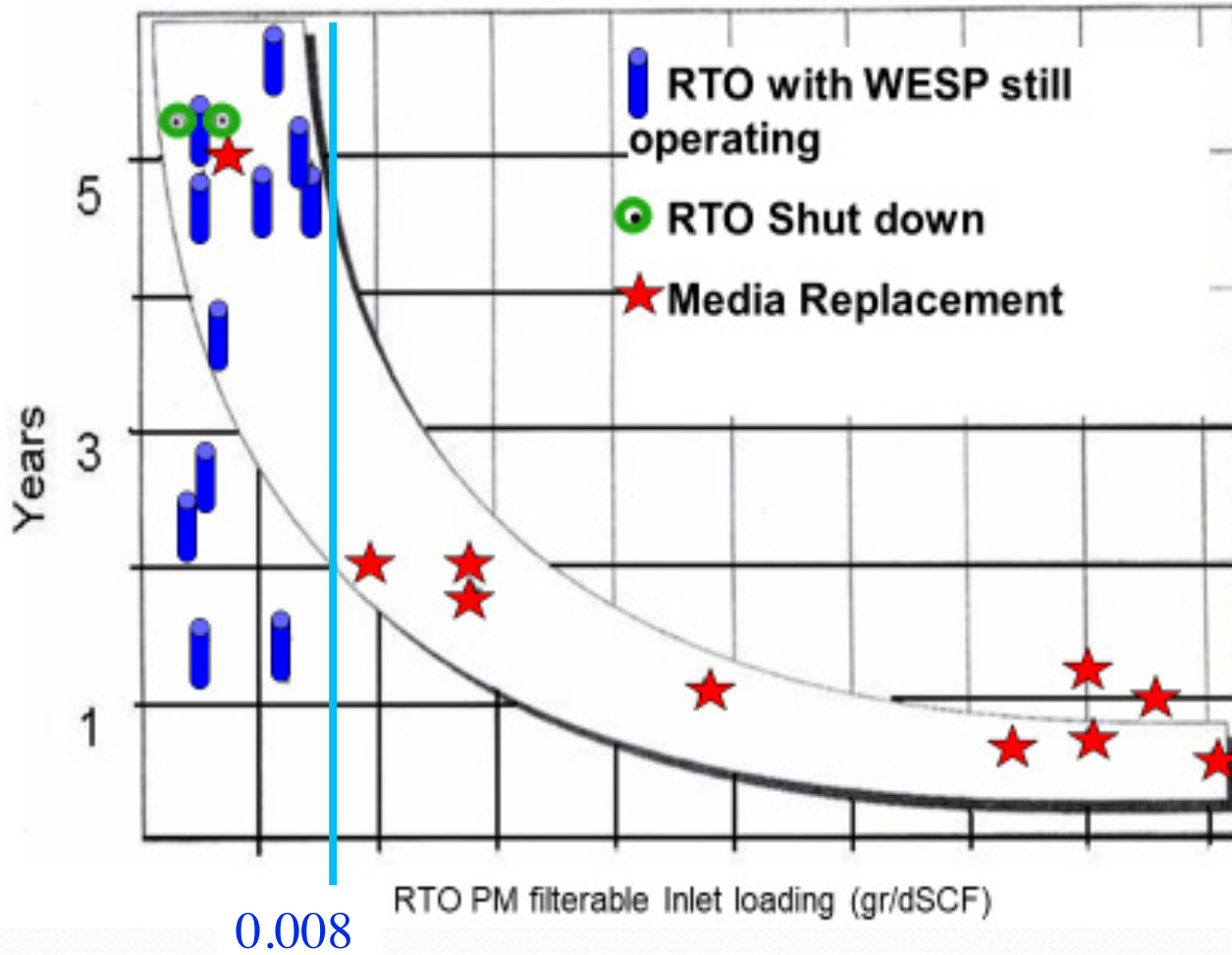


## **WESP water management key for maximum performance**

- Separate cleaner water streams from the dirty streams
- Recirculation tank with sloped bottom centrifuge exhaust
- Blow down system to maintain solids less than 5%
- Heated flushing water system
- Caustic with Membrane Cell less than 75 ppm NaCL
- Demisting system to eliminate/minimize water carry over



## 2. RTO Media Life with & without PM (Fly-ash) Control On Wood fired dyer applications

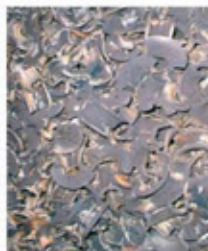




# RTO Heat Exchange Media failures

Selecting the **correct** media bed **composition** and **type** of media, including multiple media layers can eliminate or minimize RTO heat exchange problems.

- Heat exchange media plugging, degradation and fusion due to fly ash, & potassium, etc.

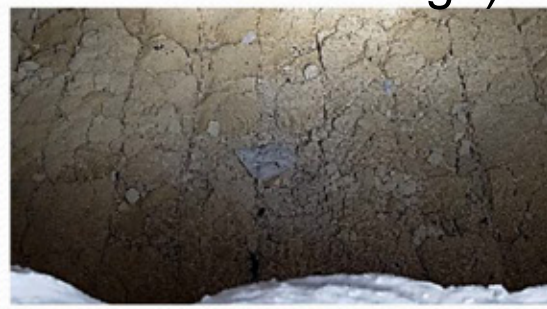


- Media Composition Percentage (%  $\text{AlO}_2$  based on fly ash )

Alumina Oxide	17-25	18-23	18-28	27.4	30 - 33	30-41	45-55	55-65
Silicon Dioxide	> 73	65-75	63-75	65	60 - 64	52-63	37-47	25-30
Sodium Oxide	4	2 - 4	1 - 4	4.1	2 - 3	0-1	0-5	0-0.5
Potassium Oxide						0-5	0-5	1-1.6



- Burner flame impingement (combustion chamber design)





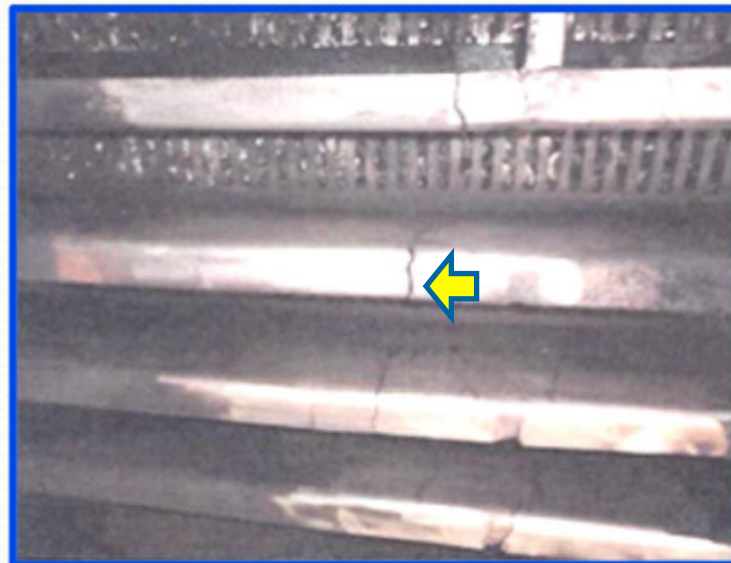
### 3. RTO Chloride-induced stress corrosion cracking (SCC) Failures

OCCURS when very specific conditions exist simultaneously:

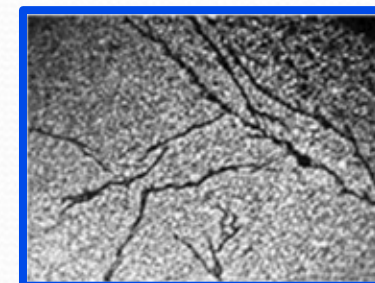
1. Chlorides present in the environment where austenitic stainless steel is being used.
2. The metal surface must be wet; that is, liquid water must be available.
3. Threshold stress must be exceeded for cracking to initiate or propagate.



Insulation anchor failure  
with 304 SS RTO



304 SS cold face SCC failures





# RTO Chloride-induced Stress Corrosion Cracking solutions

SCC can be minimized, and often eliminated entirely, by removing one or more of the necessary conditions:

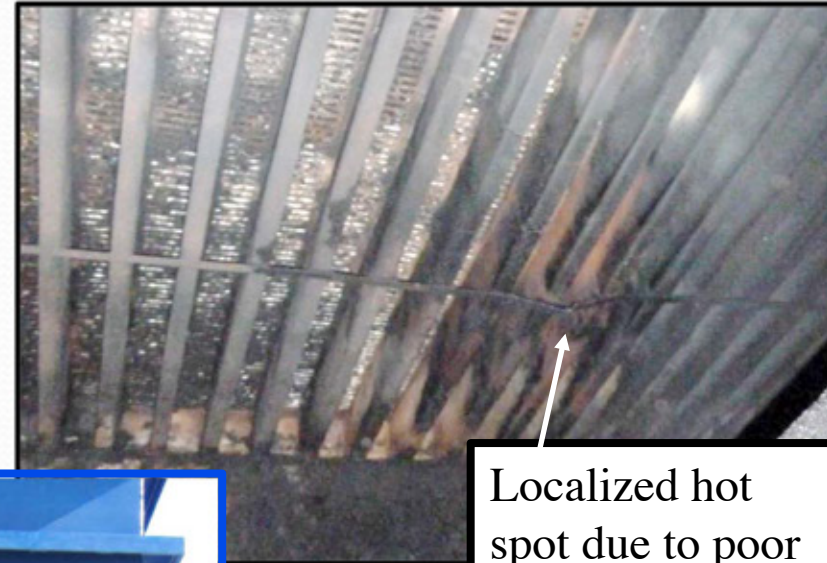
1. Use a WESP Caustic with:
  - (NaOH with Membrane Cell <75 ppm NaCL)
2. Minimize WESP water droplet carry over to RTO
  - Small droplets after WESP ..... < 5 micron
  - Chevron with uniform flow
    - Sizing
    - Washing frequency with ~ 3.5 gpm/ft<sup>2</sup> at 30 psi at spray nozzles
3. Install a moisture barrier and/or use a stainless steel with high resistance to Stress Corrosion Cracking.
4. Located media supports out of the process flow. (proprietary design)



## 4. RTO Media Support Failures



Thermal expansion not accounted for



Localized hot spot due to poor flow distribution



Easy access & inspection from both sides of MCC RTO chamber

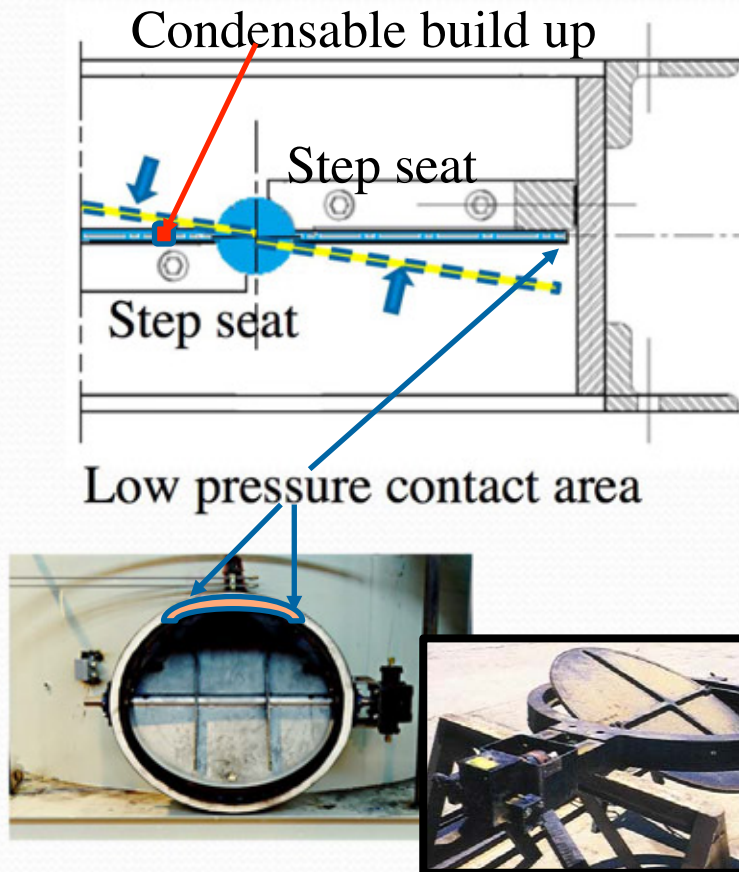
Cold face nozzles float and can expand in all directions during bake outs

External beam support



## 5. Flow Control Valve Failures

### Butterfly Valve



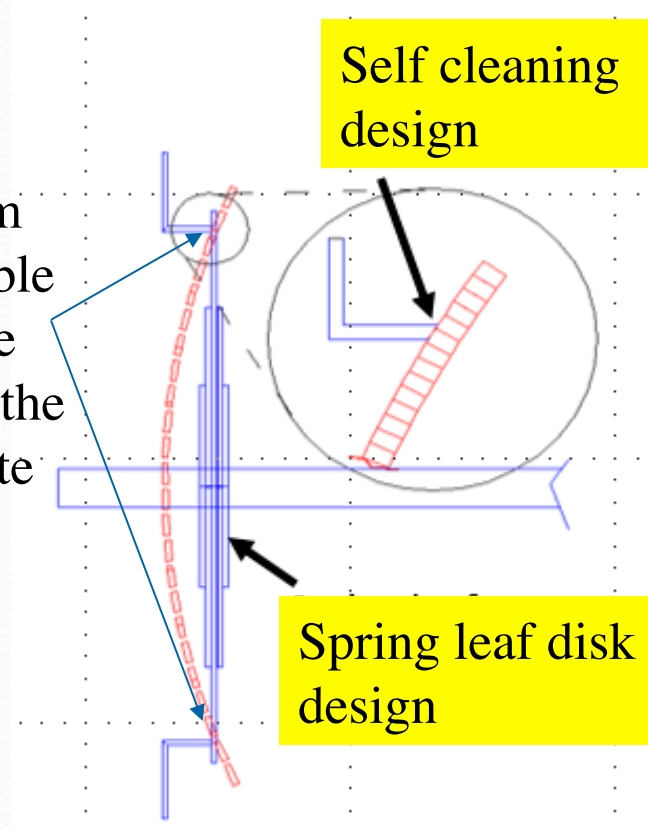
### Poppet Valve

Horizontal shaft

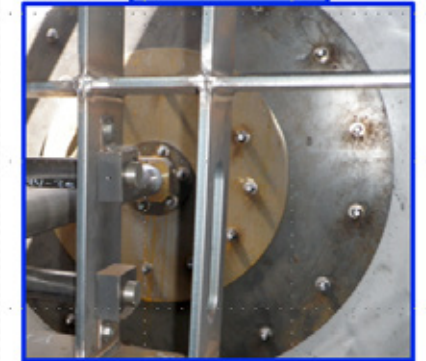
Uniform adjustable pressure around the complete seat

Self cleaning design

Spring leaf disk design



Spring Leaf Disk

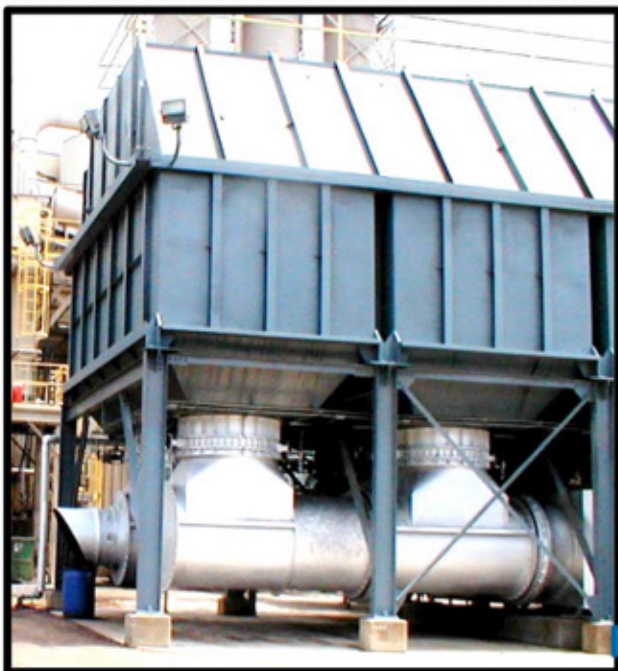


Spring Leaf Disk





# Replace hydraulic butterfly valves with pneumatic Poppet valves



Slide poppet valve assembly under heat exchange chambers

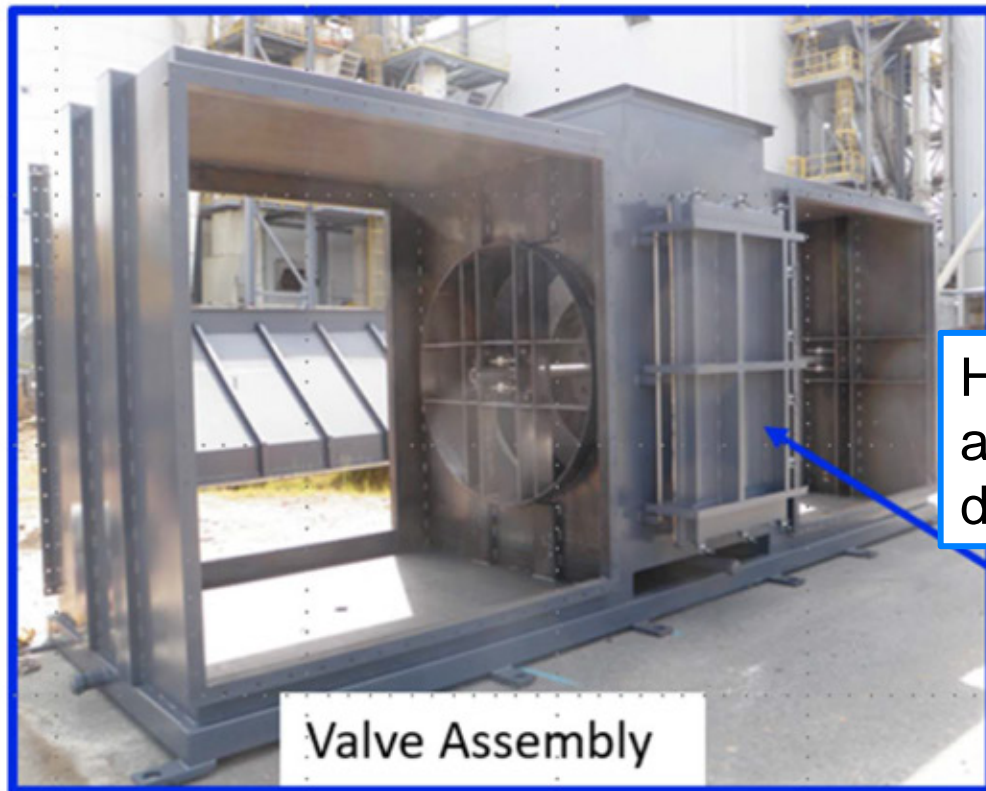


From this to this or this





# Easy Access for inspection and/or maintenance of Flow Control Valves



Hinged  
access  
door





Existing seven (7) chamber single combustion chamber, hydraulic butterfly valve RTO up graded to a MCC (multi-combustion chamber) RTO design.

Several new features were added to reduce the overall operating costs and improve reliable uptime operation. Original **104,000 wSCFM** with 95% DRE, tested at **152,000 wSCFM** at 96.7% DRE on CO and VOCs.

- Replaced and/or repair needed components identified from inspection.
- Replaced hydraulic butterfly with pneumatic poppet valves
- Replaced media cold face support
- Added flow distribution nozzles with uniform air distribution
- Add on line bake out system, no production down time
- Added thermal Energy alignment for Energy savings



Existing seven (7) chamber single combustion chamber RTO up  
graded to a six (6) chamber MCC (multi-combustion chamber) RTO



From this 7 chamber



To this 6 chamber MCC





Combustion chamber  
converted to the MCC  
RTO Design





# Up graded burner system



From this

To this — with ground level controls



Individual  
combustion  
chamber control-  
uniform  
temperature with  
fuel savings





**RTO/RCO on line bake out can be schedule on a frequency requirement based on the specific RTO needs rather than on available process down time.**

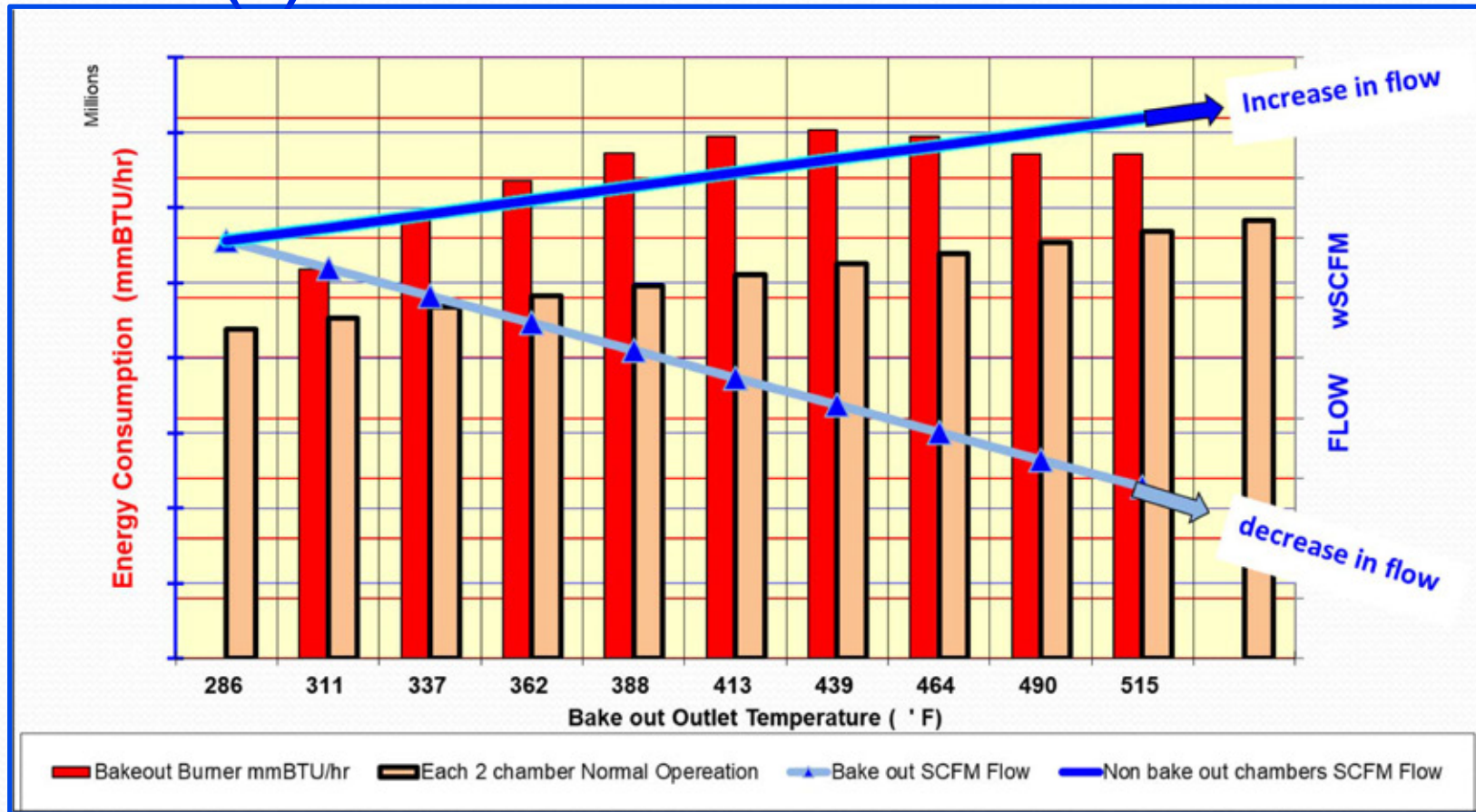
On Line Bake out;

- provides a significant savings in lost production time,
- virtually eliminate the potential for large accumulations of organic material in the RTO/RCO,
- essentially eradicate the associated potential for run-away fires that typically occur with offline bake outs due to excessive organic build within the RTO/RCO,
- substantially reduce the energy consumption that is associated with off line bake out.
- 1/3 of the Bake out exhaust is mixed with the other 2/3 normal flow up the stack



# RTO/RCO on line Bake Out

## One (1) of the 2 chamber section at a time





Thanks for your Attention.  
If you have specific questions or would like  
additional information, please see us at our  
Booth #216 or the NESTEC web site.

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